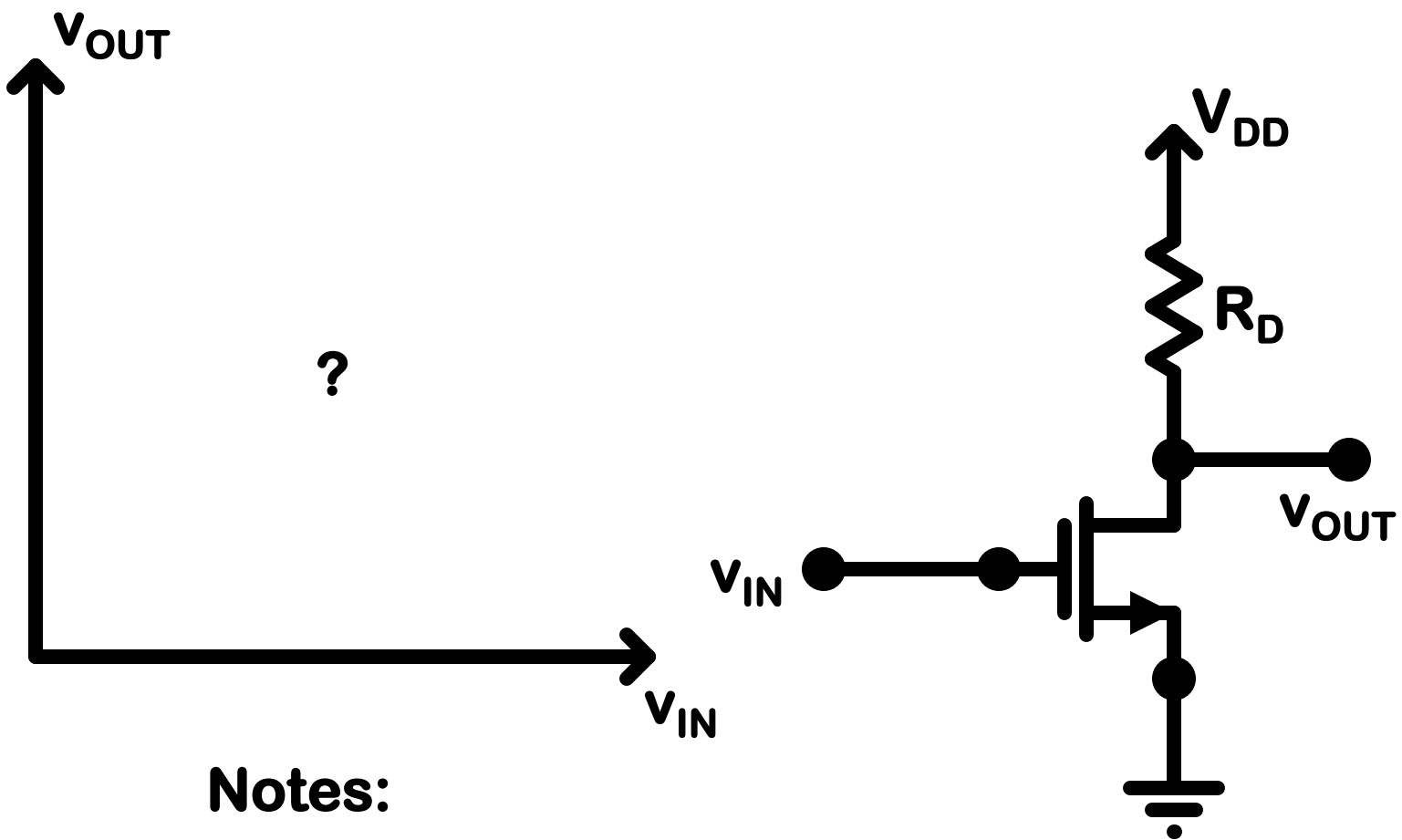


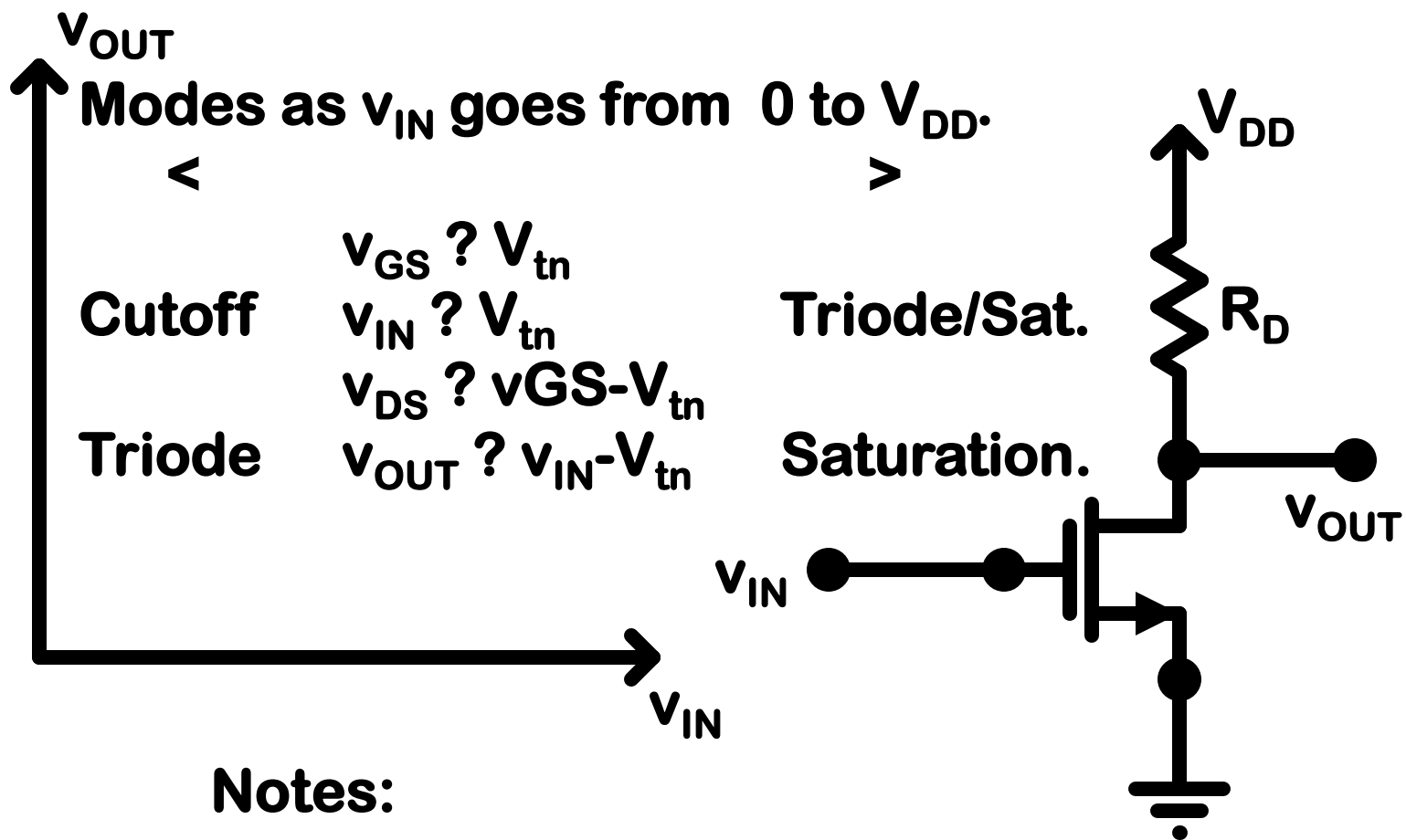


Notes:

$$v_{IN} = v_{GS}$$

$$v_{OUT} = v_{DS} = V_{DD} - R_D i_D$$

As v_{IN} (or v_{GS}) increases from zero to V_{DD} .

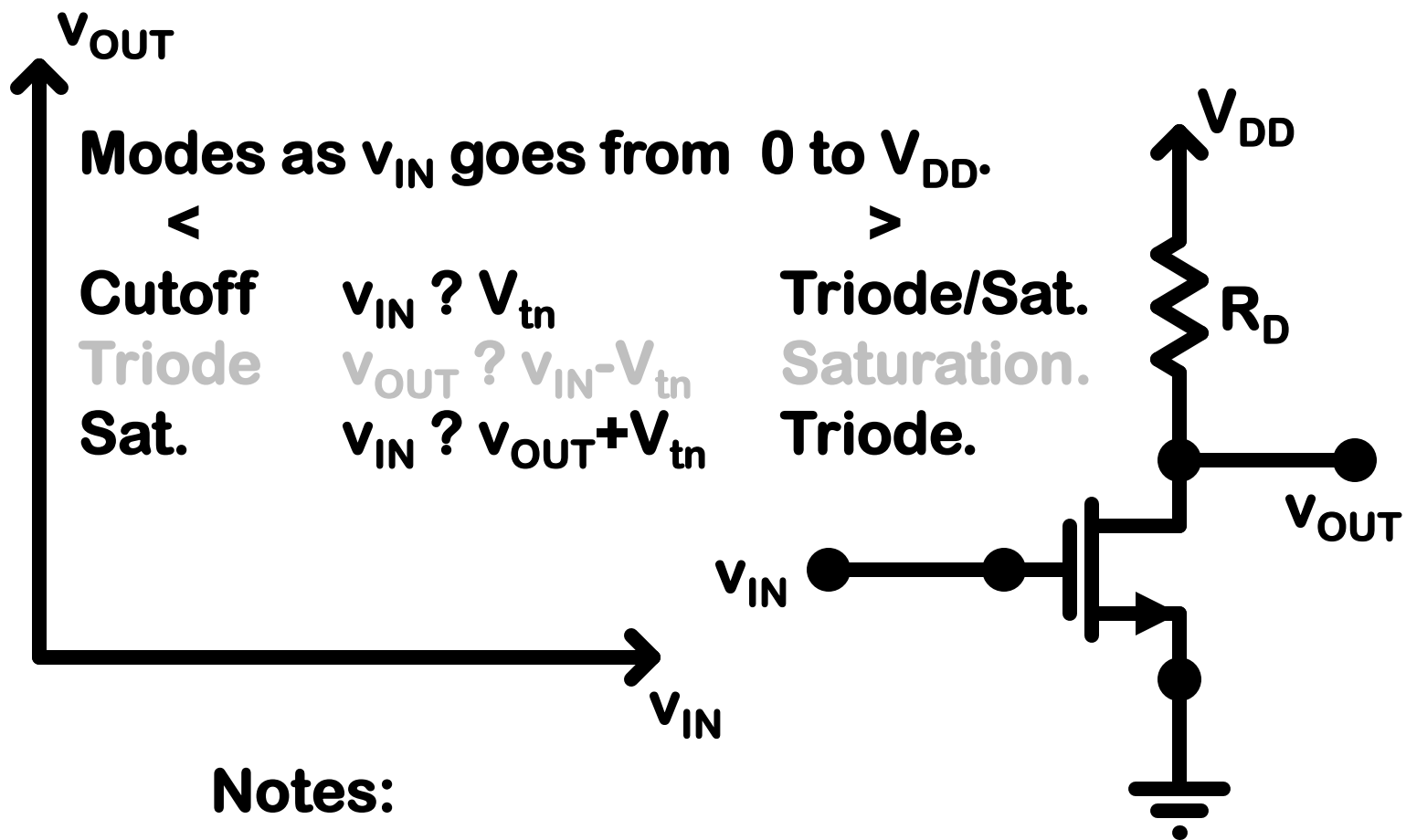


Notes:

$$v_{IN} = v_{GS}$$

$$v_{OUT} = v_{DS} = V_{DD} - R_D i_D$$

As v_{IN} (or v_{GS}) increases from zero to V_{DD} .

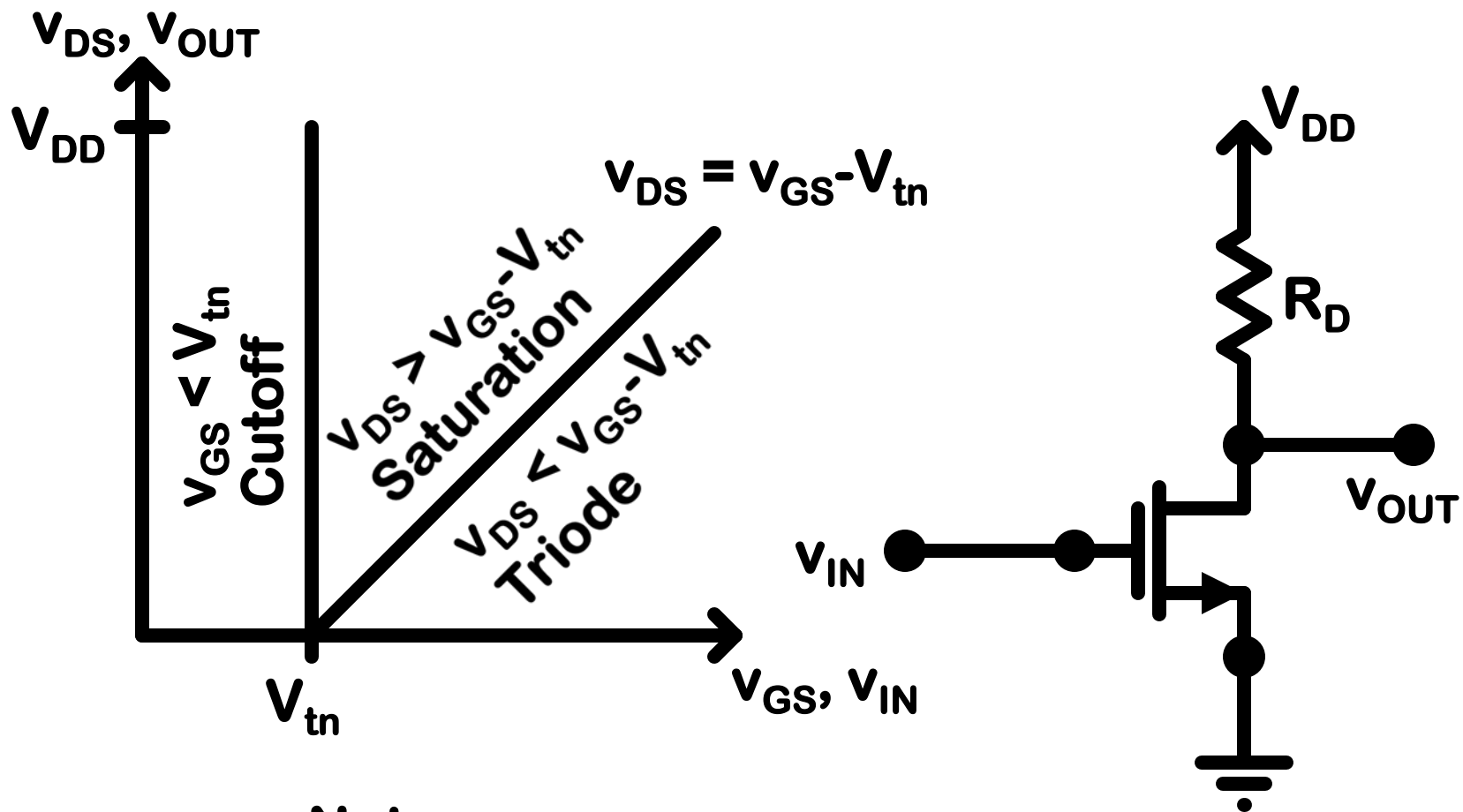


Notes:

$$v_{IN} = v_{GS}$$

$$v_{OUT} = v_{DS} = V_{DD} - R_D i_D$$

As v_{IN} (or v_{GS}) increases from zero to V_{DD} .

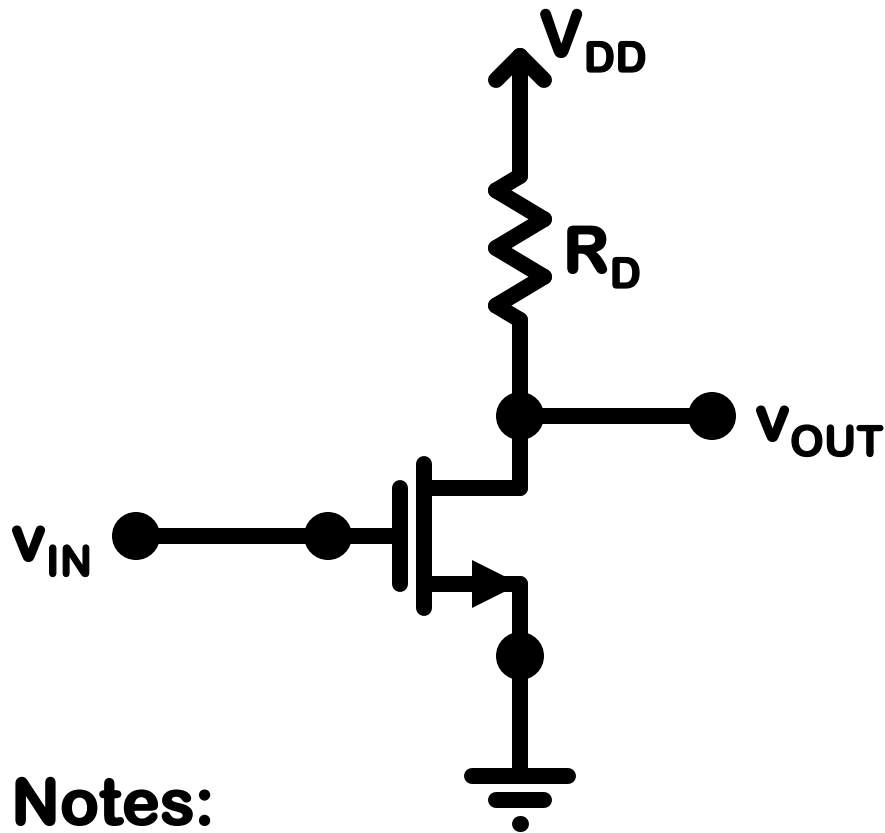


Notes:

$$V_{IN} = V_{GS}$$

$$V_{OUT} = V_{DS} = V_{DD} - R_D i_D$$

**As v_{IN} (or v_{GS}) increases from zero to V_{DD} .
Modes: cutoff, saturation, triode**



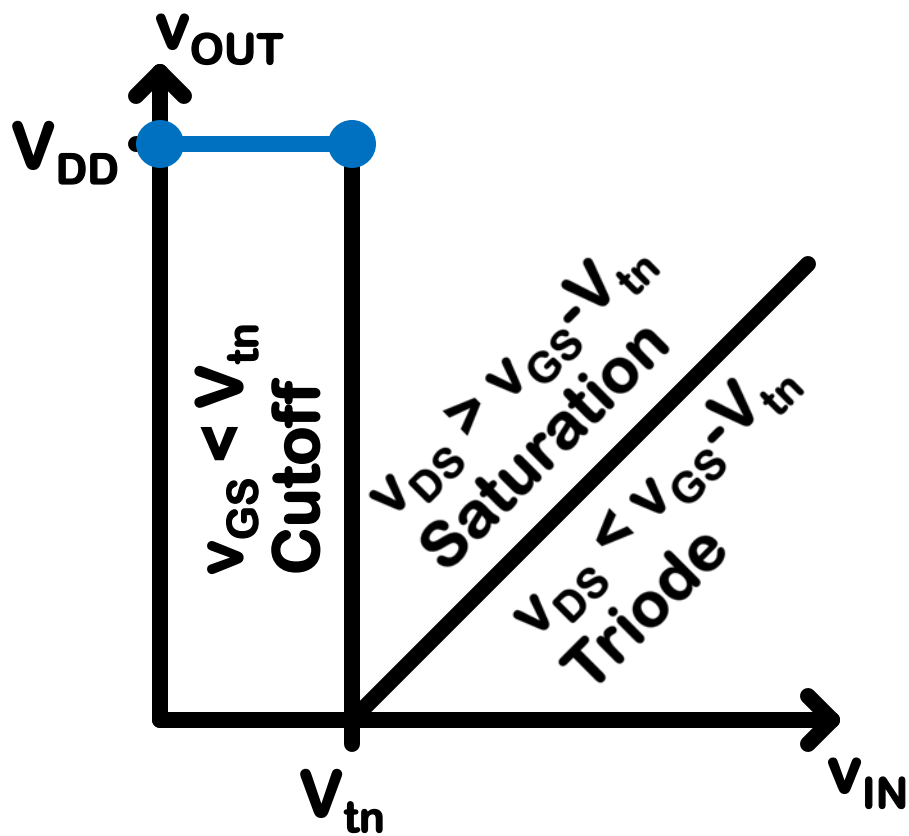
Notes:

$$V_{IN} = V_{GS}$$

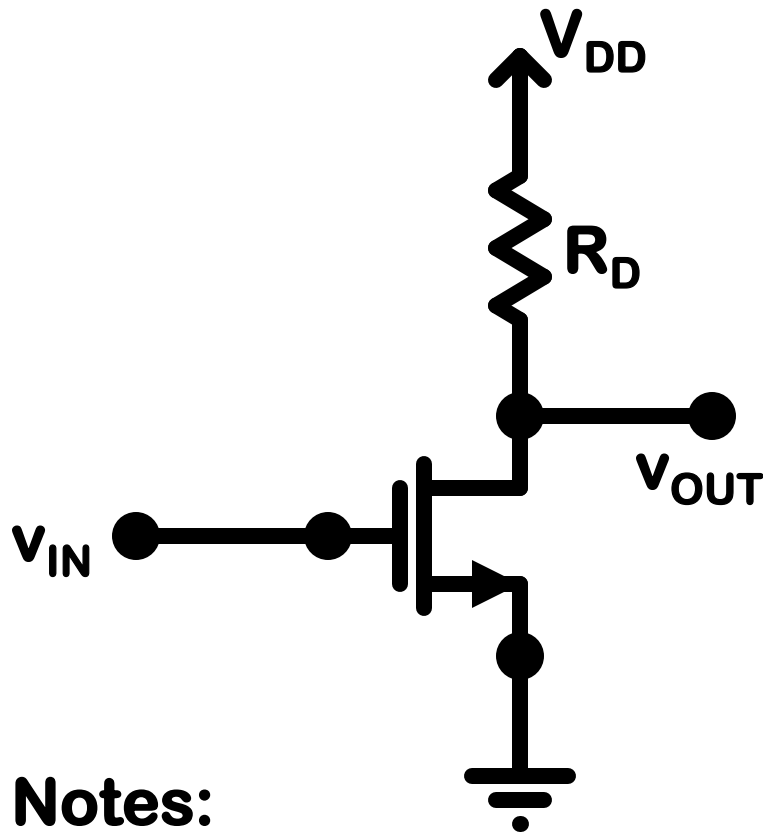
$$V_{OUT} = V_{DS} = V_{DD} - R_D i_D$$

1. Cutoff Mode:
2. $i_D = 0$
3. $v_{OUT}(v_{IN}) = V_{DD}$
4. $v_{GS} - V_{tn} < 0$
 $v_{IN} < V_{tn}$

$$v_{OUT}(v_{IN}) = V_{DD} \text{ for } v_{IN} < V_{tn}$$



$$v_{OUT}(v_{IN}) = V_{DD} \text{ for } v_{IN} < V_{tn}$$



Saturation Mode:
Device Parameter:

$$k_n = k_n' (W/L)$$

$$i_D = 0.5k_n(v_{GS} - V_{tn})^2$$

$$v_{OUT}(v_{IN}) = V_{DD} - R_D 0.5k_n(v_{IN} - V_{tn})^2$$

$$v_{GS} - V_{tn} > 0$$

$$v_{IN} > V_{tn}$$

Notes:

$$v_{IN} = v_{GS}$$

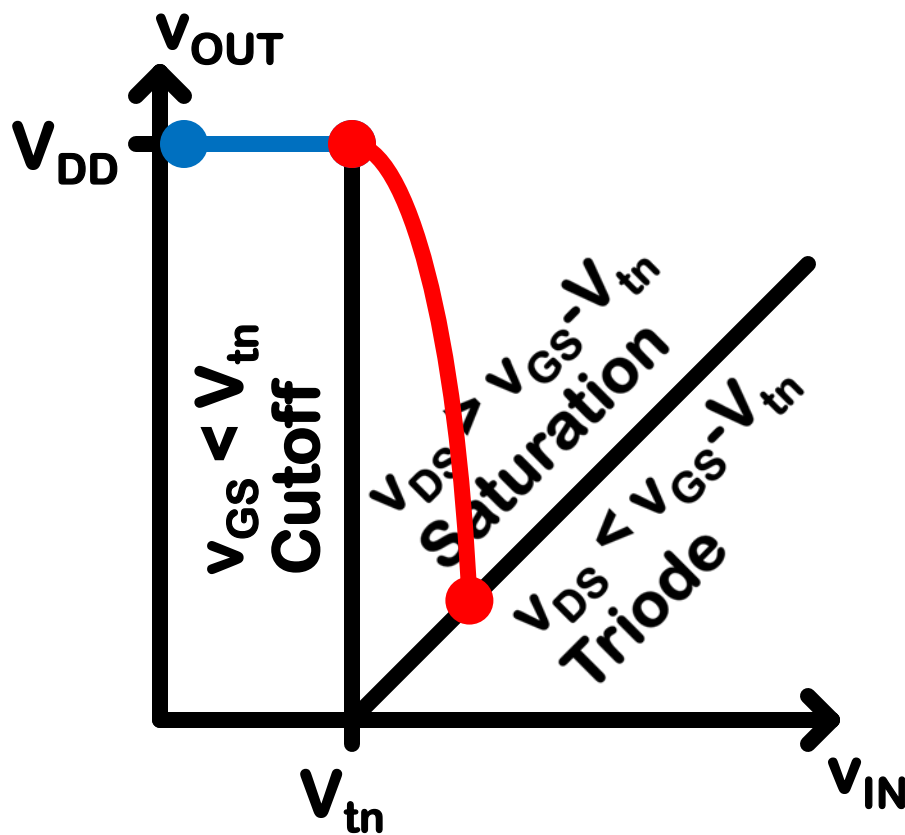
$$v_{OUT} = v_{DS} = V_{DD} - R_D i_D$$

$$v_{DS} > v_{GS} - V_{tn}$$

$$V_{DD} - R_D 0.5k_n(v_{IN} - V_{tn})^2 > v_{IN} - V_{tn}$$

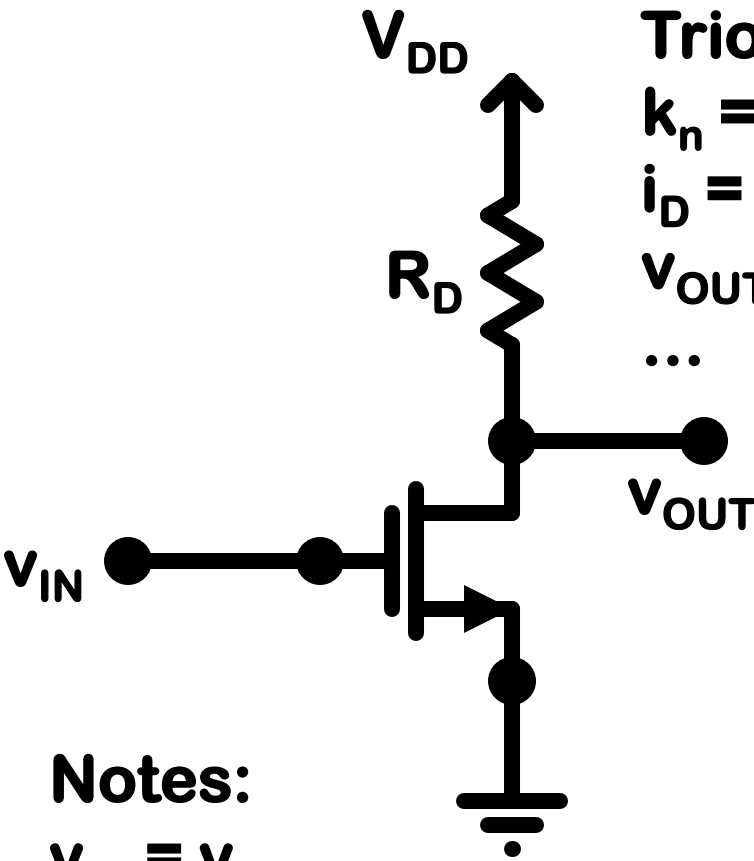
$$v_{IN} < V_{tn} + ((1 + 2R_D k_n V_{DD})^{1/2} - 1) / R_D k_n$$

$$v_{OUT}(v_{IN}) = V_{DD} - R_D 0.5k_n(v_{IN} - V_{tn})^2 \text{ for } V_{tn} < v_{IN} < V_{tn} + ((1 + 2R_D k_n V_{DD})^{1/2} - 1) / R_D k_n$$



$$v_{OUT}(v_{IN}) = V_{DD} \text{ for } v_{IN} < V_{tn}$$

$$v_{OUT}(v_{IN}) = V_{DD} - R_D 0.5 k_n (v_{IN} - V_{tn})^2 \text{ for } V_{tn} < v_{IN} < V_{tn} + ((1 + 2R_D k_n V_{DD})^{1/2} - 1) / R_D k_n$$



Triode Mode:

$$k_n = k_n' (W/L)$$

$$i_D = k_n (v_{GS} - V_{tn} - 0.5v_{DS})v_{DS}$$

$$v_{OUT} = V_{DD} - R_D k_n (v_{IN} - V_{tn} - 0.5v_{OUT})v_{OUT}$$

Notes:

$$v_{IN} = v_{GS}$$

$$v_{OUT} = v_{DS} = V_{DD} - R_D i_D$$

$v_{OUT}(v_{IN}) = \text{SEE NEXT PAGE for}$
 $v_{IN} > V_{tn} + ((1 + 2R_D k_n V_{DD})^{1/2} - 1) / R_D k_n$

Triode Mode:

$$k_n = k_n' (W/L)$$

$$i_D = k_n (v_{GS} - V_{tn} - 0.5v_{DS})v_{DS}$$

$$v_{OUT} = V_{DD} - R_D k_n (v_{IN} - V_{tn} - 0.5v_{OUT})v_{OUT}$$

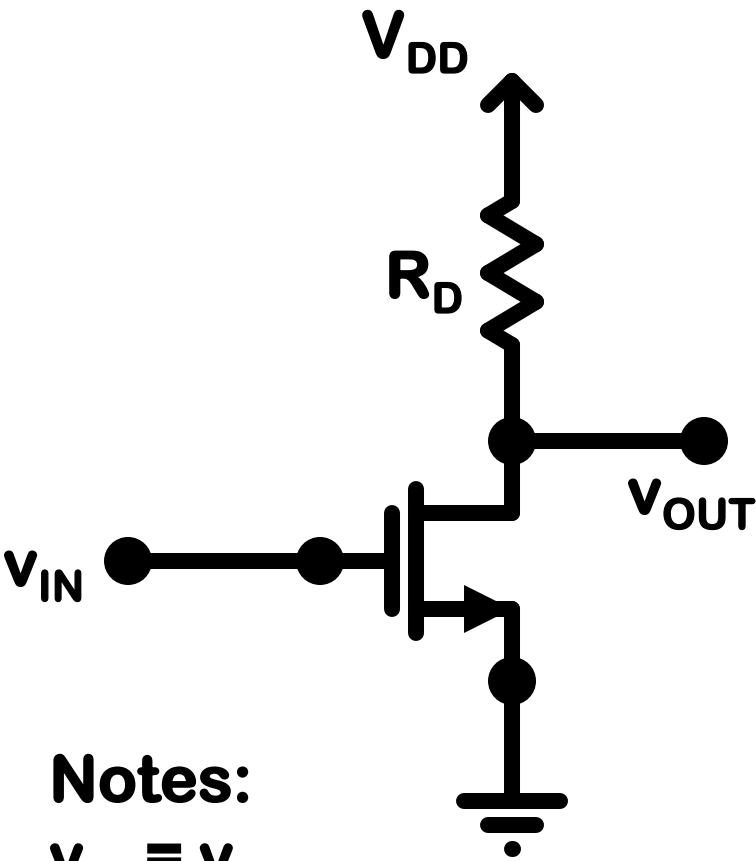
$$R_D 0.5k_n v_{OUT}^2 - (R_D k_n (v_{IN} - V_{tn}) + 1)v_{OUT} + V_{DD} = 0$$

$$a = 0.5R_D k_n$$

$$b = -(R_D k_n (v_{IN} - V_{tn}) + 1)$$

$$c = V_{DD}$$

$$v_{OUT} = (-b - \sqrt{b^2 - 4ac})/(2a)$$



Triode (small v_{DS}) Mode:

$$k_n = k_n' (W/L)$$

$$i_D = k_n (v_{GS} - V_{tn}) v_{DS}$$

$$V_{OUT} = V_{DD} - R_D k_n (v_{IN} - V_{tn}) v_{OUT}$$

$$V_{OUT} = V_{DD} / (1 + R_D k_n (v_{IN} - V_{tn}))$$

$$v_{DS} \ll v_{GS} - V_{tn}$$

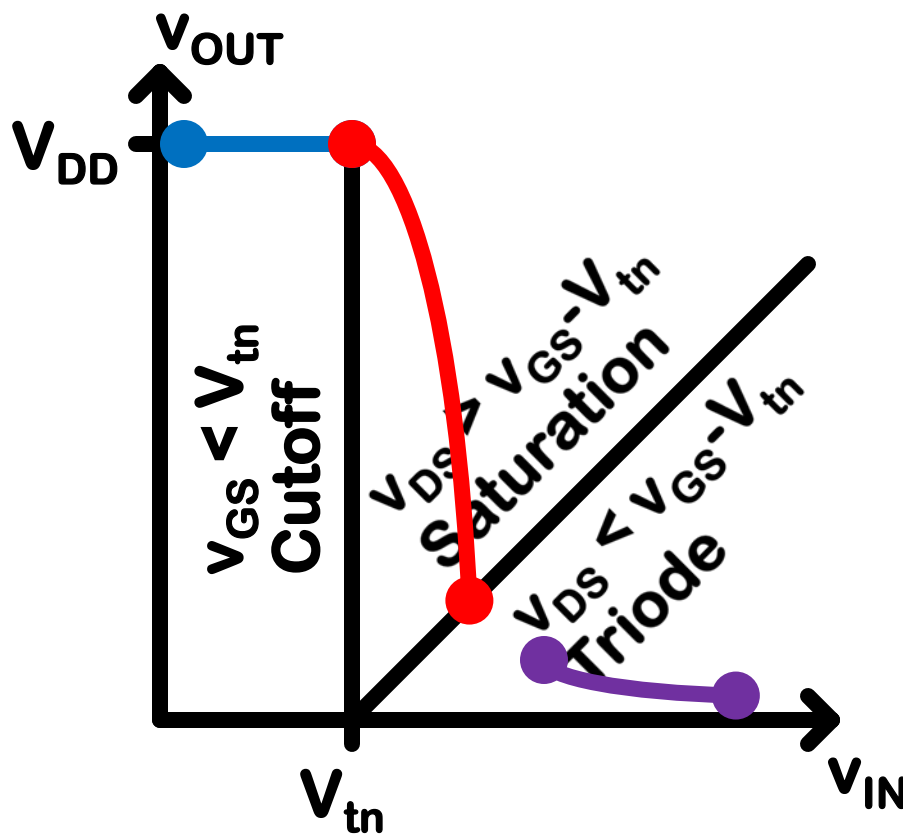
$$V_{DD} / (1 + R_D k_n (v_{IN} - V_{tn})) \ll (v_{IN} - V_{tn})$$

Notes:

$$V_{IN} = v_{GS}$$

$$V_{OUT} = v_{DS} = V_{DD} - R_D i_D$$

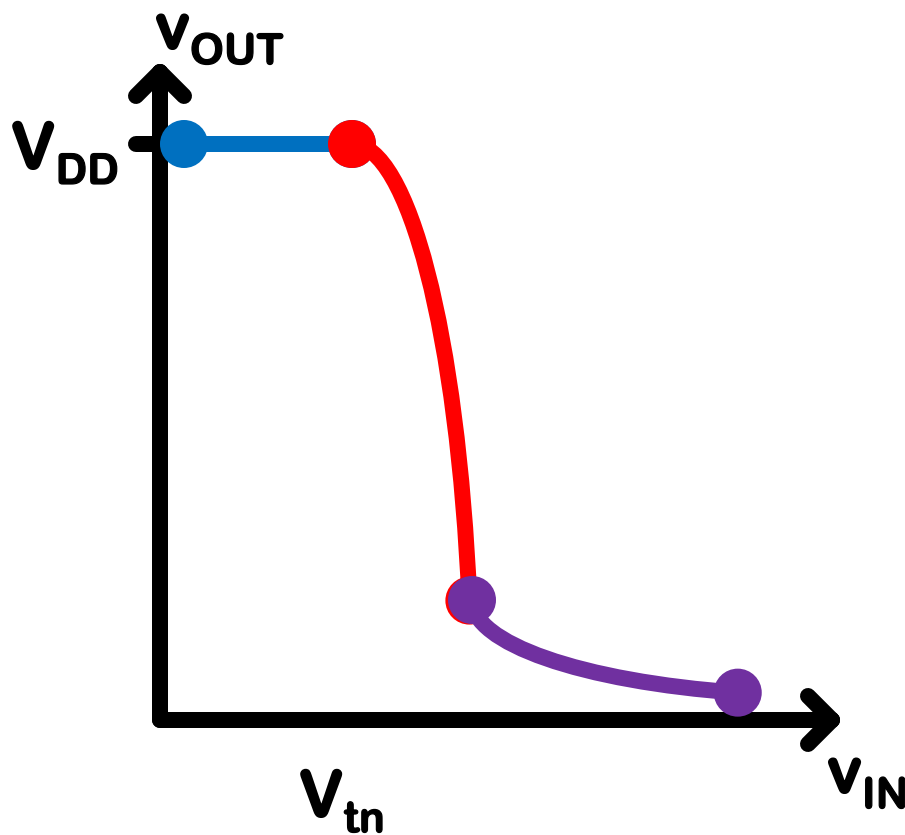
$$v_{OUT}(v_{IN}) = V_{DD} / (1 + R_D k_n (v_{IN} - V_{tn})) \text{ for } v_{IN} \gg V_{tn} + ((1 + 2R_D k_n V_{DD})^{1/2} - 1) / R_D k_n$$



$$v_{OUT}(v_{IN}) = V_{DD} \text{ for } v_{IN} < V_{tn}$$

$$v_{OUT}(v_{IN}) = V_{DD} - R_D 0.5 k_n (v_{IN} - V_{tn})^2 \text{ for } V_{tn} < v_{IN} < V_{tn} + ((1 + 2R_D k_n V_{DD})^{1/2} - 1) / R_D k_n$$

$$v_{OUT}(v_{IN}) = V_{DD} / (1 + R_D k_n (v_{IN} - V_{tn})) \text{ for } v_{IN} \gg V_{tn} + ((1 + 2R_D k_n V_{DD})^{1/2} - 1) / R_D k_n$$

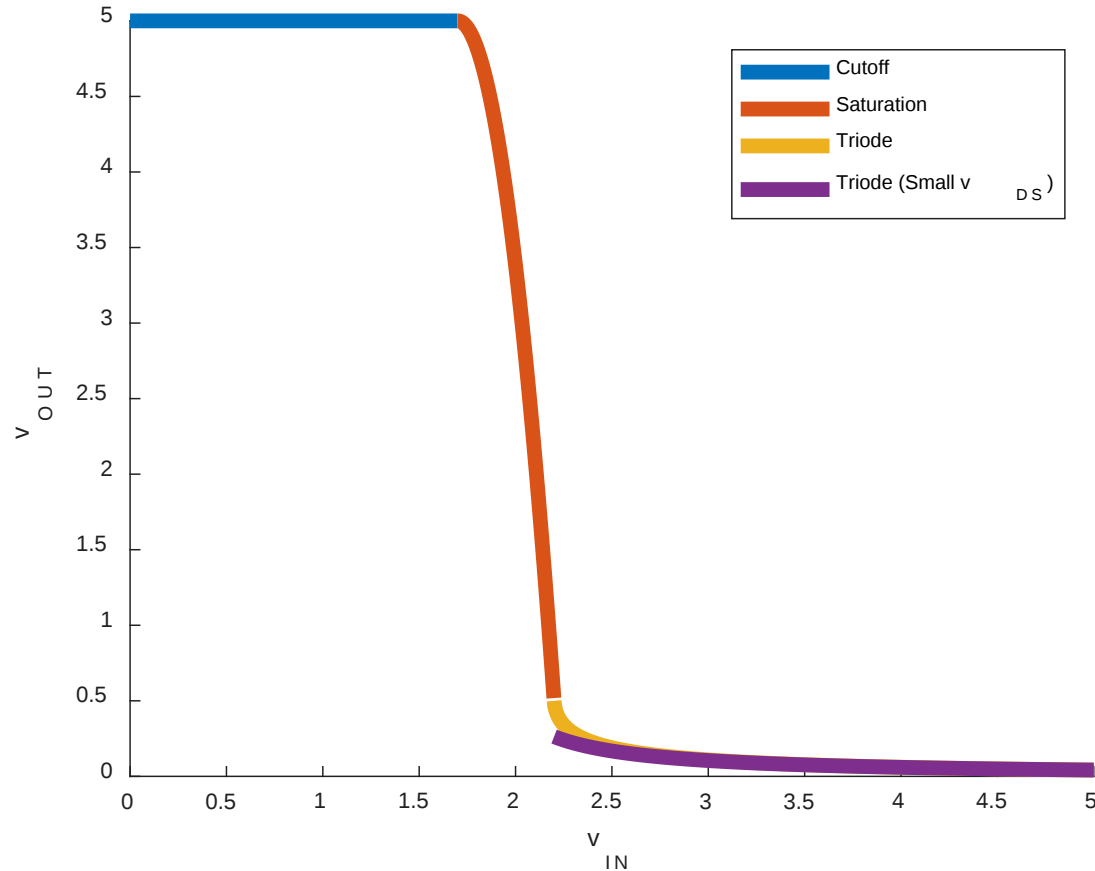


$$v_{OUT}(v_{IN}) = V_{DD} \text{ for } v_{IN} < V_{tn}$$

$$v_{OUT}(v_{IN}) = V_{DD} - R_D 0.5 k_n (v_{IN} - V_{tn})^2 \text{ for } V_{tn} < v_{IN} < V_{tn} + ((1 + 2R_D k_n V_{DD})^{1/2} - 1) / R_D k_n$$

$$v_{OUT}(v_{IN}) \approx V_{DD} / (1 + R_D k_n (v_{IN} - V_{tn})) \text{ for } v_{IN} \gg V_{tn} + ((1 + 2R_D k_n V_{DD})^{1/2} - 1) / R_D k_n$$

NMOS Inverter/Amplifier



Cutoff:

$$v_{OUT}(v_{IN}) = V_{DD}$$

for $v_{IN} < V_{tn}$

Saturation:

$$v_{OUT}(v_{IN}) = V_{DD} - R_D 0.5 k_n (v_{IN} - V_{tn})^2$$

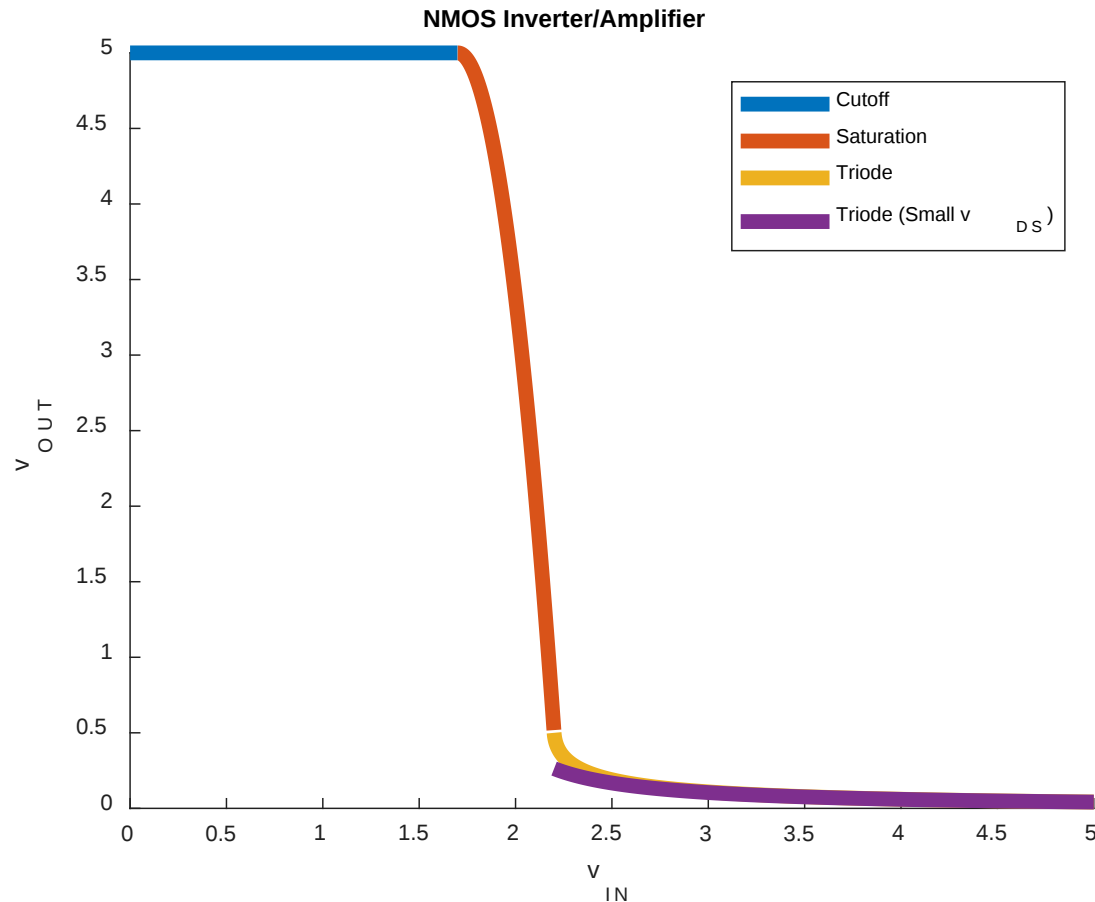
for $V_{tn} < v_{IN} < V_{tn} + ((1 + 2R_D k_n V_{DD})^{1/2} - 1) / R_D k_n$

Triode:

$$v_{OUT} = ((R_D k_n (v_{IN} - V_{tn}) + 1) - ((R_D k_n (v_{IN} - V_{tn}) + 1)^2 - 2R_D k_n V_{DD})^{1/2}) / (R_D k_n)$$

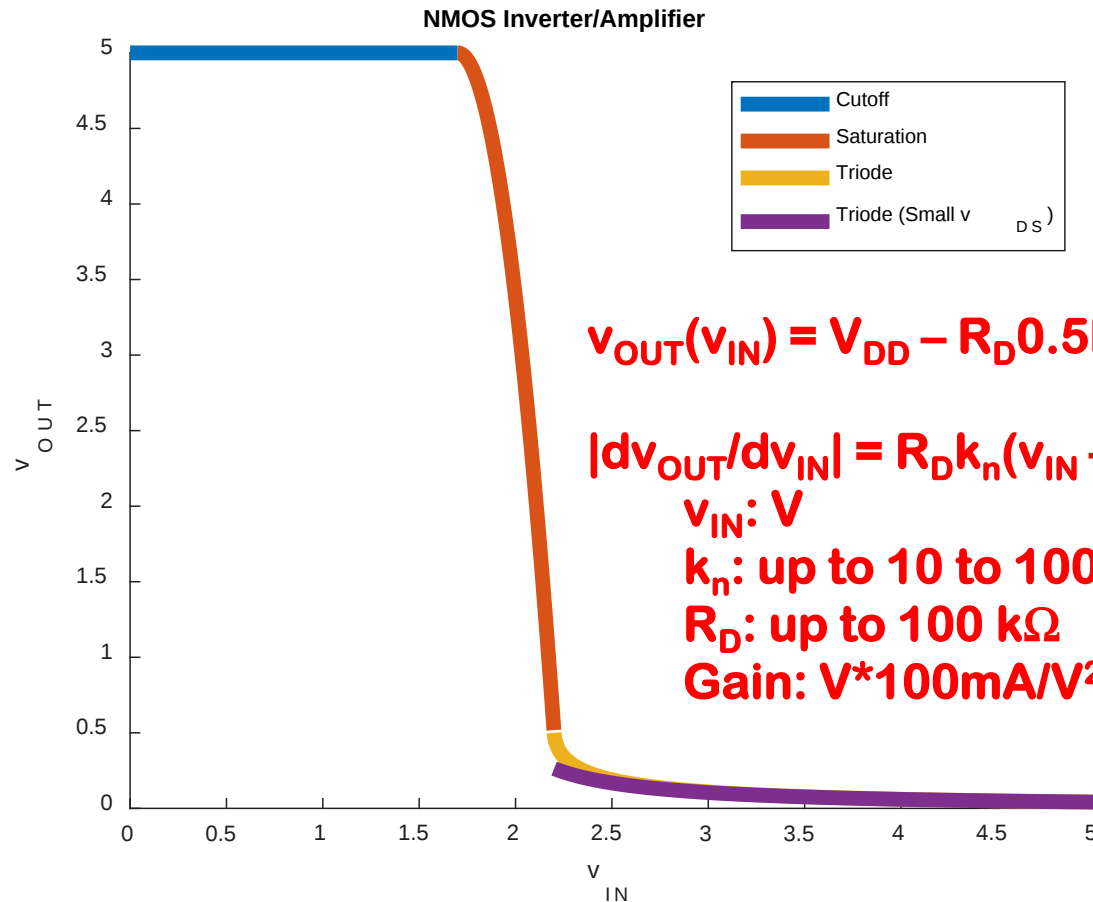
for $v_{IN} > V_{tn} + ((1 + 2R_D k_n V_{DD})^{1/2} - 1) / R_D k_n$

MOSFETs can be used in Digital Logic Applications.



The Cutoff and Triode Regions exhibit a definite digital high or low output. Saturation region is more ambiguous and is not good for logic application.

MOSFETs can be used Amplifier (Analog Applications).



$$v_{OUT}(v_{IN}) = V_{DD} - R_D 0.5 k_n (v_{IN} - V_{tn})^2$$

$$|dv_{OUT}/dv_{IN}| = R_D k_n (v_{IN} - V_{tn})$$

$$v_{IN}: V$$

$$k_n: \text{up to } 10 \text{ to } 100+ \text{ mA/V}^2$$

$$R_D: \text{up to } 100 \text{ k}\Omega$$

$$\text{Gain: } V \cdot 100 \text{ mA/V}^2 \cdot 100 \text{ k(V/A)} = \text{very large}$$

The Saturation region exhibits a slope with a large absolute value, $|dv_{OUT}/dv_{IN}| \gg 1$ (can't be done with passive components). In this region, small variations in the input will result in large variations in the output.

MOSFETs can be used Amplifier (Analog Applications).

